### Filter Design Techniques

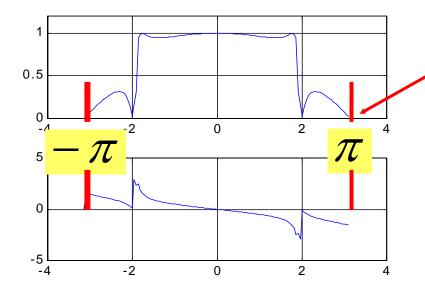
- Filter
  - Filter is a system that passes certain frequency components and totally rejects all others
- · Stages of the design filter
  - Specification of the desired properties of the system
  - Approximation of the specification using a causal discrete-time system
  - Realization of the system

# Review of discretetime systems



#### Frequency response:

- periodic: period =  $2\pi$
- for a real impulse response h[k] Magnitude response  $\left|H\left(e^{j\omega}\right)\right|$  is even function Phase response  $\angle H(e^{j\omega})$  is odd function
- example:



#### Nyquist frequency

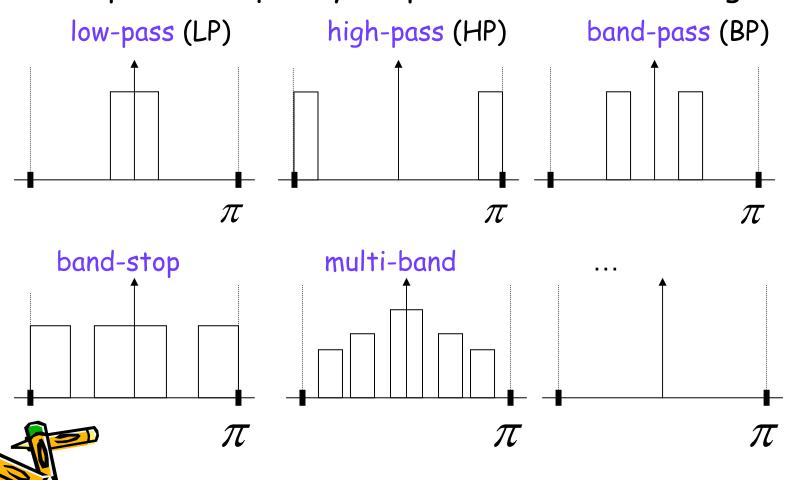
$$e^{j\pi k} = ...,1,-1,1,-1,1,...$$



# Review of discretetime systems



`Popular' frequency responses for filter design:



# Review of discretetime systems



"FIR filters" (finite impulse response):

$$H(z) = \frac{B(z)}{z^{N}} = b_0 + b_1 z^{-1} + \dots + b_N z^{-N}$$

- "Moving average filters" (MA filters)
- N poles at the origin z=0 (hence guaranteed stability)
- N zeros (zeros of B(z)), "all zero" filters
- corresponds to difference equation

$$y[k] = b_0 u[k] + b_1 u[k-1] + ... + b_N u[k-N]$$

impulse response

$$h[0] = b_0, h[1] = b_1, ..., h[N] = b_N, h[N+1] = 0, ...$$

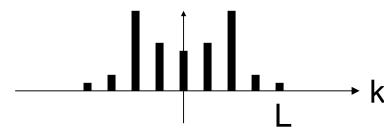




#### Non-causal zero-phase filters:

example: symmetric impulse response

$$h[k]=h[-k], k=1..L$$

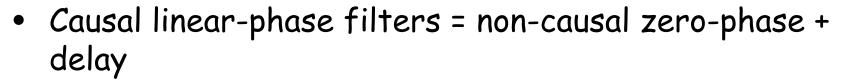


frequency response is

$$H(e^{j\omega}) = \sum_{k=-L}^{+L} h[k]e^{-j\omega . k} = \dots = \sum_{k=0}^{L} a_k \cos(\omega k)$$

- i.e. real-valued (=zero-phase) transfer function
- causal implementation by introducing (group) delay





example: symmetric impulse response & N even

N=2L (even)

h[k]=h[N-k], k=0..L

frequency response is



$$H(e^{j\omega}) = \sum_{k=0}^{N} h[k]e^{-j\omega . k} = \dots = e^{-j\omega L} \sum_{k=0}^{L} a_k \cos(\omega k)$$

= i.e. causal implementation of zero-phase filter, by introducing (group) delay  $z^{-L}\Big|_{z=e^{j\omega}}=e^{-j\omega L}$ 





Type-1 N=2L=even symmetric h[k]=h[N-k]

$$e^{-j\omega N/2}\sum_{k=0}^{L}a_k\cos(\omega k)$$

LP/HP/BP

Type-2 N=2L+1=odd symmetric h[k]=h[N-k]

$$e^{-j\omega N/2} \sum_{k=0}^{L} a_k \cos(\omega k) \qquad e^{-j\omega N/2} \cos(\frac{\omega}{2}) \sum_{k=0}^{L} a_k \cos(\omega k) \qquad j e^{-j\omega N/2} \sin(\omega) \sum_{k=0}^{L-1} a_k \cos(\omega k) \qquad j e^{-j\omega N/2} \sin(\frac{\omega}{2}) \sum_{k=0}^{L} a_k \cos(\omega k)$$

zero at  $\omega=\pi$ 

LP/BP

Type-3 N=2L=even anti-symmetric h[k]=-h[N-k]

$$je^{-j\omega N/2}\sin(\omega)\sum_{k=0}^{L-1}a_k\cos(\omega k)$$

zero at  $\omega=0,\pi$ 

Type-4 N=2L+1=odd anti-symmetric h[k]=-h[N-k]

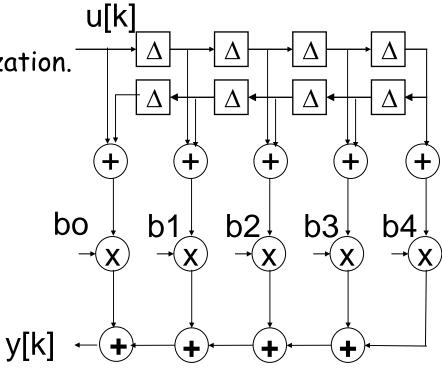
$$j.e^{-j\omega N/2}\sin(\frac{\omega}{2})\sum_{k=0}^{L}a_{k}\cos(\omega k)$$

zero at 
$$\omega = 0$$

HP



efficient direct-form realization.
 example:

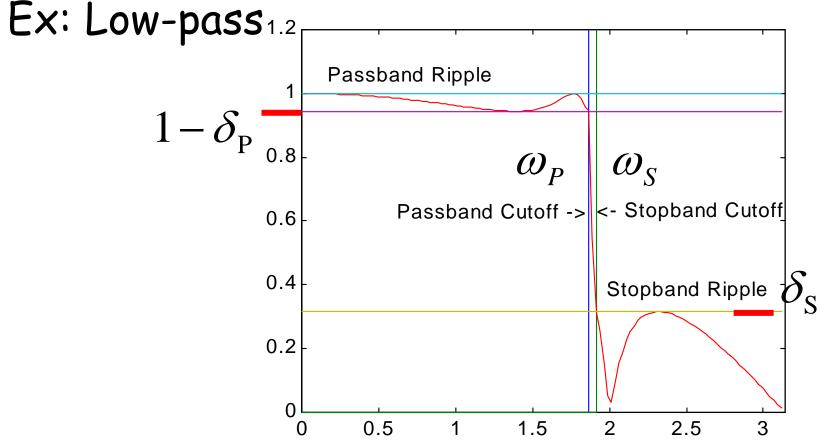


• PS: IIR filters can NEVER have linear-phase property!



## Filter Specification







### Filter Design Problem

- Design of filters is a problem of function approximation
- For FIR filter, it implies polynomial approximation
- For IIR filter, it implies approximation by a rational function of z





#### (I) Weighted Least Squares Design:

select one of the basic forms that yield linear phase

e.g. Type-1 
$$H(e^{j\omega}) = e^{-j\omega N/2} \sum_{k=0}^{L} a_k \cos(\omega k) = e^{-j\omega N/2} A(\omega)$$

specify desired frequency response (LP,HP,BP,...)

$$H_d(\omega) = e^{-j\omega N/2} A_d(\omega)$$

• optimization criterion is

$$\min_{a_0,\dots,a_L} \int_{-\pi}^{+\pi} W(\omega) \Big| H(e^{j\omega}) - H_d(\omega) \Big|^2 d\omega = \min_{a_0,\dots,a_L} \int_{-\pi}^{+\pi} W(\omega) \Big| A(\omega) - A_d(\omega) \Big|^2 d\omega$$

$$F(a_0,\dots,a_L)$$

where  $W(\omega) \ge 0$  is a weighting function



• ...this is equivalent to

$$\min_{x} \{ x^{T} Q x - 2x^{T} p + \mu \}$$

$$x^{T} = \begin{bmatrix} a_{0} & a_{1} & \dots & a_{L} \end{bmatrix}$$

$$Q = \int_{0}^{\pi} W(\omega) c(\omega) c^{T}(\omega) d\omega$$

$$p = \int_{0}^{\pi} W(\omega) A_{d}(\omega) c(\omega) d\omega$$

$$c^{T}(\omega) = \begin{bmatrix} 1 & \cos(\omega) & \dots & \cos(L\omega) \end{bmatrix}$$

$$\mu = \dots$$

=standard 'Quadratic Optimization' problem

$$x_{OPT} = Q^{-1}p$$





Passband Ripple

Passband Cutoff -> <- Stopband Cutoff

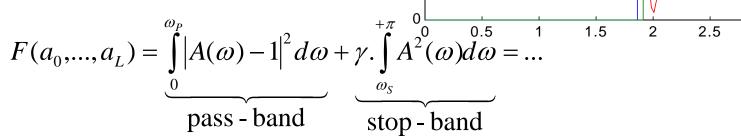
Stopband Ripple

Example: Low-pass design

$$A_d(\omega) = 1, |\omega| < \omega_P$$
 (pass - band)

$$A_d(\omega) = 0, \omega_S \le |\omega| \le \pi$$
 (stop - band)

optimization function is



0.8

0.6

0.4

0.2

i.e.

$$W(\omega) = ...$$



a simpler problem is obtained by replacing the F(..) by...

$$\underline{F}(a_0, ..., a_L) = \sum_{i} W(\omega_i) |A(\omega_i) - A_d(\omega_i)|^2 = \sum_{i} W(\omega_i) \left\{ c^T(\omega_i) \begin{bmatrix} a_0 \\ \vdots \\ a_L \end{bmatrix} - A_d(\omega_i) \right\}^2$$

where the wis are a set of n sample frequencies

The quadratic optimization problem is then equivalent to a least-squares problem

$$\min_{x} \left\| \underline{A}x - \underline{b} \right\|_{2}^{2} = \min_{x} \left\{ x^{T} \underbrace{\underline{A}^{T}\underline{A}}_{\sum_{i} W(\omega_{i})c(\omega_{i})c^{T}(\omega_{i})} x - 2x^{T} \underbrace{\underline{A}^{T}\underline{b}}_{\sum_{i} \dots} + \underbrace{\underline{b}^{T}\underline{b}}_{\sum_{i} \dots} \right\}$$

$$x_{LS} = (\underline{A}^T \underline{A})^{-1} \underline{A}^T \underline{b}$$
 Compare to p.12

+++ : simple

--: unpredictable behavior in between sample frequencies.

• ...then all this is often supplemented with additional constraints

Example: Low-pass (LP) design (continued) pass-band ripple control:

 $|A(\omega)-1| \le \delta_{\rm P}, |\omega| < \omega_{\rm P}$  ( $\delta_{\rm P}$  is pass - band ripple)

stop-band ripple control:

 $|A(\omega)| \le \delta_{\rm S}, \omega_{\rm S} \le |\omega| \le \pi$  ( $\delta_{\rm S}$  is stop - band ripple)





Example: Low-pass (LP) design (continued)

a realistic way to implement these constraints, is to impose the constraints (only) on a set of sample frequencies

 $\omega_{P1},\omega_{P2},...,\omega_{Pm}$  in the pass-band

and  $\omega_{S1}, \omega_{S2}, ..., \omega_{Sn}$  in the stop-band

The resulting optimization problem is:

minimize:  $F(a_0,...,a_L) = ...$ 

$$x^T = \begin{bmatrix} a_0 & a_1 & \dots & a_L \end{bmatrix}$$

subject to  $A_P x \le b_P$  (pass-band constraints)

 $A_S x \le b_S$  (stop-band constraints)

= `Quadratic Linear Programming' problem



### (II) `Minimax' Design:

• select one of the basic forms that yield linear phase

e.g. Type-1 
$$H(e^{j\omega}) = e^{-j\omega N/2} \sum_{k=0}^{L} a[k] \cos(\omega k) = e^{-j\omega N/2} A(\omega)$$

• specify desired frequency response (LP,HP,BP,...)

$$H_d(\omega) = e^{-j\omega N/2} A_d(\omega)$$

optimization criterion is

$$\min_{a_0,\dots,a_L} \max_{0 \le \omega \le \pi} W(\omega) \Big| H(e^{j\omega}) - H_d(\omega) \Big| = \min_{a_0,\dots,a_L} \max_{0 \le \omega \le \pi} W(\omega) \Big| A(\omega) - A_d(\omega) \Big|$$

where  $W(\omega) \ge 0$  is a weighting function



- Conclusion:
  - (I) weighted least squares design
    (II) minimax design
    provide general `framework', procedures to
    translate filter design problems into standard
    optimization problems
- In practice (and in textbooks):
   emphasis on specific (ad-hoc) procedures :
  - filter design based on 'windows'
  - equi-ripple design



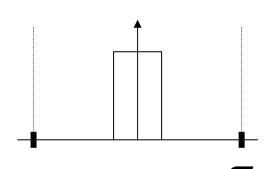


#### Filter Design using 'Windows'



ideal low-pass filter is

$$H_d(\omega) = \begin{cases} 1 & |\omega| < \omega_C \\ 0 & \omega_C < |\omega| < \pi \end{cases}$$



hence ideal time-domain impulse response is

$$h_d[k] = \frac{1}{2\pi} \int_{-\pi}^{+\pi} H_d(e^{j\omega}) e^{j\omega_{.k}} d\omega = \dots = \alpha \frac{\sin(\omega_c k)}{\omega_c k}$$

truncate h<sub>d</sub>[k] to N+1 samples :

$$h[k] = \begin{cases} h_d[k] & -N/2 < k < N/2 \\ 0 & \text{otherwise} \end{cases}$$

add (group) delay to turn into causal filter



### Filter Design using 'Windows'

Example: Low-pass filter design (continued)

- note: it can be shown that time-domain truncation corresponds to solving a weighted least-squares optimization problem with the given  $H_d$ , and weighting function  $W(\omega)=1$
- truncation corresponds to applying a 'rectangular window';

$$h[k] = h_d[k]w[k]$$

$$w[k] = \begin{cases} 1 & -N/2 < k < N/2 \\ 0 & \text{otherwise} \end{cases}$$

- +++: simple procedure (also for HP,BP,...)
- ---: truncation in the time-domain results in 'Gibbs effect' in the frequency domain, i.e. large ripple in pass-band and stop-band, which cannot be reduced by increasing the filter order N.

### Filter Design using 'Windows'

#### Remedy: apply windows other than rectangular window:

 time-domain multiplication with a window function w[k] corresponds to frequency domain convolution with W(z):

$$h[k] = h_d[k]w[k]$$

$$H(z) = H_d(z) * W(z)$$

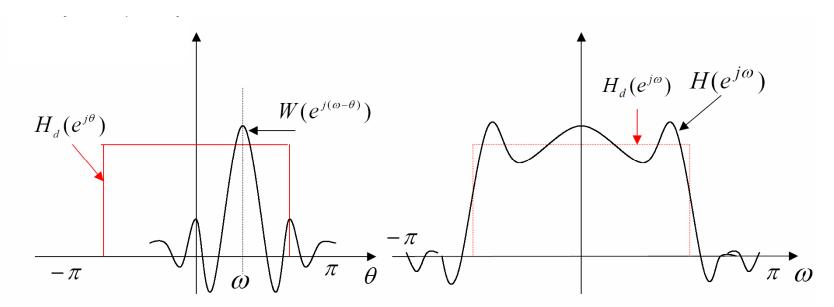
- candidate windows: Han, Hamming, Blackman, Kaiser,.... (see textbooks)
- window choice/design = trade-off between side-lobe levels (define peak pass-/stop-band ripple) and width main-lobe (defines transition bandwidth)





# Windowing Effect

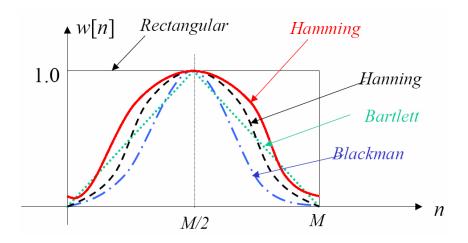


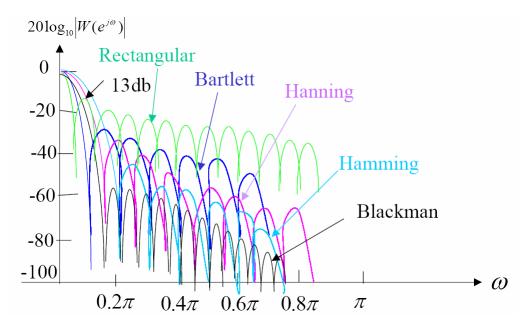


Gibbs phenomenon



### Windowing









### Equiripple Design



Starting point is minimax criterion, e.g.

$$\min_{a_0,\dots,a_L} \max_{0 \leq \omega \leq \pi} W(\omega) \Big| A(\omega) - A_d(\omega) \Big| = \min_{a_0,\dots,a_L} \max_{0 \leq \omega \leq \pi} \Big| E(\omega) \Big|$$

 Based on theory of Chebyshev approximation and the 'alternation theorem', which (roughly) states that the optimal a<sub>i</sub>'s are such that the 'max' (maximum weighted approximation error) is obtained at L+2 extremal frequencies...

$$\max_{0 \le \omega \le \pi} |E(\omega)| = |E(\omega_i)| \quad \text{for } i = 1,..,L+2$$

...that hence will exhibit the same maximum ripple ('equiripple')

- Iterative procedure for computing extremal frequencies, etc. (Remez exchange algorithm, Parks-McClellan algorithm)
- Very flexible, etc., available in many software packages
- Details omitted here (see textbooks)



#### Software

- FIR Filter design abundantly available in commercial software
- Matlab:

b=fir1(n,Wn,type,window), windowed linear-phase FIR design, n is filter order, Wn defines band-edges, type is `high',`stop',...

b=fir2(n,f,m,window), windowed FIR design based on inverse Fourier transform with frequency points f and corresponding magnitude response m

b=remez(n,f,m), equiripple linear-phase FIR design with Parks-McClellan (Remez exchange) algorithm



